

# The 'Double' Michaelis-Menten Equation: Estimation of Parameters

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Z. Naturforsch. **38 c**, 268–272 (1983); received September 9, 1982/January 5, 1983

Sum of Two Michaelis-Menten Terms, Integrated Rate Equation, Parameter Estimation

When the concentration dependence of an enzymic reaction or a transport process can be described by the sum of two Michaelis-Menten terms, reliable data that relate reaction rate and substrate concentration can be obtained even when as much as 70 per cent of substrate was consumed during the assay. Each data pair consists of the average reaction rate during an assay and the concentration where the instantaneous reaction rate was equal to the average rate. Although that concentration cannot be computed exactly (as it depends on the four kinetic parameters), it may be computed in a good approximation as if the reaction followed the simple Michaelis-Menten relationship. The relative error in the approximated concentration for  $1 \leq K_2/K_1 \leq 10^5$  and  $10^{-2} \leq V_2/V_1 \leq 10^2$  did not exceed 5 per cent up to 50 per cent of substrate consumption, and did not exceed 10 per cent up to 70 per cent of substrate consumption.

## Introduction

In general, initial reaction rates, or uptake rates, are measured at various substrate concentrations to determine the Michaelis constant ( $K$ ) and the maximal reaction rate ( $V$ ) of an enzyme preparation or a transport process. In some cases it may be convenient, or even necessary to measure an average reaction rate over a time interval in which the substrate concentration had decreased considerably. If during the assay the substrate concentration decreased from  $S_0$  at zero time to  $S_1$  at time  $t_1$ , the average reaction rate is given by  $(S_0 - S_1)/t_1$ . According to the Theorem of the Mean some value of  $S$  exists in the interval where the instantaneous reaction rate is equal to the average rate. If the process obeys the Michaelis-Menten equation, the value of that concentration equals  $(S_0 - S_1)/\ln(S_0/S_1)$ , as can be derived from the integrated form of that equation [1, 2].

In some enzymological studies [3, 4] and in many transport studies [5, 6] it has been found that the concentration dependence of the reaction rate can be described by the sum of two Michaelis-Menten terms. In such a system one can again ask for the concentration where the instantaneous reaction rate equals the average rate over a time interval. This

problem is considerably more complicated than the single-reaction case (see Appendix). When the double reaction is treated as if it were a single reaction, however, it can be demonstrated that the resulting error is small for quite a large range of values of the four parameters involved,  $K_1$ ,  $K_2$ ,  $V_1$ , and  $V_2$ . In addition it is shown that the estimation of these parameters is hardly affected by this procedure.

## Results and Discussion

In case of two, simultaneously occurring Michaelis-Menten reactions, the concentration,  $S_x$ , where the instantaneous reaction rate equals the average rate over a time interval  $(0, t_1)$  depends on  $S_0$  and  $S_1$ , but also on the kinetic parameters  $K_1$ ,  $K_2$ ,  $V_1$ , and  $V_2$  [see Appendix, Eqn. (7)]. As the latter parameters are unknown one has to find a good approximation which is independent of these parameters.

When  $S_x$  is calculated as if we were dealing with a single reaction,

$$S_x \approx \tilde{S}_x = (S_0 - S_1)/\ln(S_0/S_1)$$

the relative error,  $q$ , in  $\tilde{S}_x$  may be defined by

$$q = (S_x/\tilde{S}_x) - 1.$$

Since  $\tilde{S}_x/S_0$  depends on  $S_1/S_0$ , and since  $S_x/S_0$  is a function of the ratios  $S_1/S_0$ ,  $S_0/K_1$ ,  $K_2/K_1$ , and  $V_2/V_1$  [see Appendix, Eqn. (8)] it follows that  $q$  is a function of these ratios as well. Accordingly, the

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0341-0382/83/0300-0268 \$ 01.3 0/0



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Table I. Values of the ratios  $K_2/K_1$  and  $V_2/V_1$  in some enzyme preparations and transport functions.

	Biological material	$K_2/K_1$	$V_2/V_1$	Ref.
Enzyme				
Ornithine decarboxylase	<i>Physarum polycephalum</i>	130	10	[4]
3':5'-cyclic nucleotide phosphodiesterase	rat liver	130	60	[3]
Transport function				
K <sup>+</sup>	barley roots	540	1	[9]
D-glucose	hamster small intestine	20	1	[10]
D-glucose	<i>Neocosmospora vasinfecta</i>	130	1	[11]
D-galactose	rat intestine	10	2	[12]
L-leucine	cultured mouse cells	10	3	[13]
L-leucine	duckweed	330	5	[14]
L-histidine	<i>Salmonella typhimurium</i>	650	5	[15]
L-histidine	baker's yeast	20	3	[16]
L-histidine	S37 ascites tumor cells	70	6	[17]

relative error  $\varrho$  in  $\tilde{S}_x$  was computed for various values of these ratios. Some realistic values of  $K_2/K_1$  and  $V_2/V_1$  are listed in Table I.

Fig. 1 shows, for  $K_2/K_1 = 100$  and  $V_2/V_1 = 10$ , the increase in the error in  $\tilde{S}_x$  as the reaction proceeds. At various initial substrate concentrations the error is smaller than 4 per cent up to a substrate consumption of 70 per cent ( $S_1/S_0 = 0.3$ ). Fig. 1 also indicates that  $\varrho$  strongly depends on the initial substrate concentration. The error is largest when  $S_0/K_1$  has some value between 1 and  $K_2/K_1$ , thus when  $S_0$  has some value between  $K_1$  and  $K_2$ . This is depicted

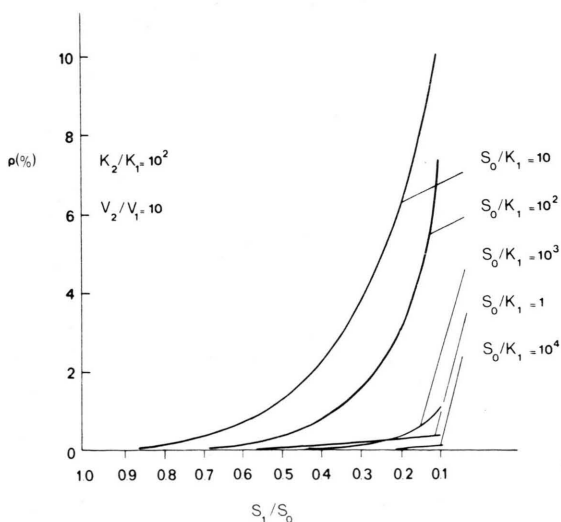


Fig. 1. Relative error ( $\varrho$ ) in  $\tilde{S}_x$  at various initial substrate concentration  $S$  ( $S_0/K_1$ ) as a function of the progress of the reaction ( $S_1/S_0$ ).

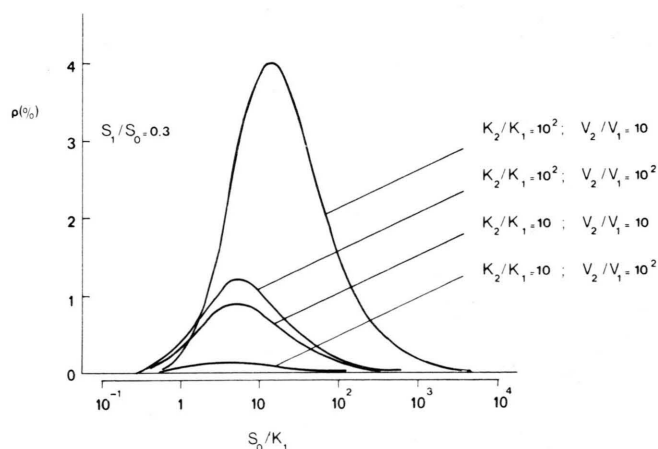


Fig. 2. Relative error ( $\varrho$ ) in  $\tilde{S}_x$  as a function of the initial substrate concentration ( $S_0/K_1$ ) at 70 per cent substrate consumption ( $S_1/S_0 = 0.3$ ) and various values of  $K_2/K_1$  and  $V_2/V_1$ .

more clearly in Fig. 2, where  $\varrho$  is presented as a function of  $S_0/K_1$  at several values of  $K_2/K_1$  and  $V_2/V_1$ , and a substrate consumption of 70 per cent.

A detailed presentation of the dependence of  $\varrho$  on  $K_2/K_1$  and  $V_2/V_1$  at various initial substrate concentrations and 70 per cent substrate consumption is given in Fig. 3.

We investigated to what extent the values of the kinetic parameters to be estimated may be affected by the use of the approximate value  $\tilde{S}_x$ . As can be seen in Table II (data set (a)), deviations in the estimated parameters were less than 2 per cent in most cases, and never were larger than 5 per cent.

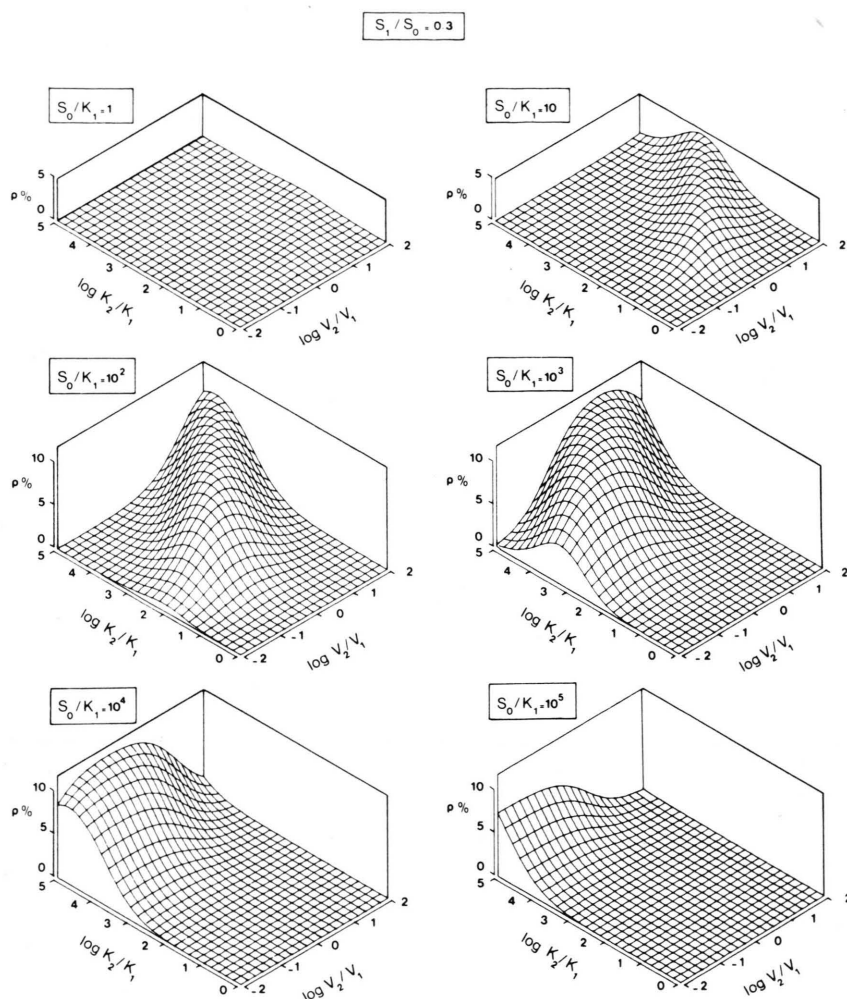


Fig. 3. Relative error ( $\rho$ ) in  $\hat{S}_x$  at 70 per cent substrate consumption ( $S_1/S_0 = 0.3$ ) and various values of  $S_0/K_1$ , as a function of  $K_2/K_1$  and  $V_2/V_1$ .

Parameter estimation may be disturbed, however, by 'experimental' error in the reaction rates. For example, a 5 per cent 'experimental' error resulted in poor estimation of the parameters  $K_1$  and  $V_1$  when  $K_2/K_1 = 10$  and  $V_2/V_1 = 10$  or  $V_2/V_1 = 100$ , or when  $K_2/K_1 = 100$  and  $V_2/V_1 = 100$ . This was found for the data set of average reaction rates ( $\bar{r}$ ) and the matching approximated values of substrate concentrations ( $\hat{S}_x$ ), as well as for the data set of initial substrate concentrations and reaction rates (Table II, data sets (b) and (c), respectively). The poor estimation of parameter-values in these cases, therefore, is not due to the use of  $\hat{S}_x$ . As has been pointed out by Gross et al. [7] it results from the limitations of

kinetic analysis at certain constellations of  $K_2/K_1$ ,  $V_2/V_1$ , and the relative error in the data.

We conclude that the procedure described in this paper may be safely used to collect data from the determination of the parameters of the 'double' Michaelis-Menten equation. The restriction to be made is that during the assay the relationship between concentration and reaction rate should not change. Thus, enzyme reactions should be practically irreversible, and product inhibition or progressive denaturation of the enzyme should not occur. Similarly, in uptake experiments efflux should be negligible, and the influx may not be affected by transinhibition during the assay.

Table II. Deviations in the kinetic parameters due to the use of the approximate value  $\tilde{S}_x = (S_0 - S_1)/\ln(S_0/S_1)$ . The sum of two Michaelis-Menten terms was fitted to sets of simulated data, essentially as described by Cleland [8]. Each set consists of 25 data pairs; initial concentrations were spaced geometrically between 0.1  $K_1$  and 10  $K_2$ . For each set of parameter-values, three data sets were composed: (a) Data were computed for 70 per cent substrate consumption. Reaction rates were equal to  $\bar{r} = 0.7 S_0/t$  ( $t$  being computed from Eqn. (3)), and substrate concentrations were equal to  $\tilde{S}_x = (S_0 - S_1)/\ln(S_0/S_1)$ ; (b) data were obtained as in (a), but in addition a 5 per cent random error [cf. reference 18] was assigned to the values of the reaction rates; (c) data set of substrate concentrations and reaction rates at  $t = 0$ , with a 5 per cent random error in the reaction rates.

True parameter-values				Estimated parameter-values				
$K_1$	$K_2$	$V_1$	$V_2$	$K_1$	$K_2$	$V_1$	$V_2$	
1	10	1	10	(a)	1.02	9.89	1.01	9.97
				(b)	0.64	8.48	0.53	10.2
				(c)	0.77	9.37	0.71	10.3
1	10	1	100	(a)	1.04	9.99	1.02	99.9
				(b)	1.06	11.1	1.25	104
				(c)	2.04	11.6	3.43	101
1	100	1	10	(a)	1.02	96.9	1.01	9.91
				(b)	0.97	101	0.94	9.86
				(c)	0.97	108	0.95	9.96
1	100	1	100	(a)	1.05	99.4	1.04	99.8
				(b)	0.55	89.3	0.60	95.8
				(c)	0.53	93.0	0.62	97.8
1	1000	1	10	(a)	1.01	955	1.01	9.78
				(b)	1.04	974	1.03	10.0
				(c)	1.02	1003	1.01	10.1
1	1000	1	100	(a)	1.03	983	1.03	99.4
				(b)	1.03	1030	1.06	101
				(c)	1.00	1029	1.04	100

## Appendix

In case of two, simultaneously operating, Michaelis-Menten processes, the rate of change of the substrate concentration  $S$  is described by the equation

$$v = -\frac{dS}{dt} = V_1 S/(K_1 + S) + V_2 S/(K_2 + S). \quad (1)$$

This can be rewritten as

$$\frac{1}{v} = -\frac{dt}{dS} = \alpha + \beta/S + \gamma/(\delta + S) \quad (2)$$

where  $\alpha$ ,  $\beta$ ,  $\gamma$ ,  $\delta$  are abbreviations for various combinations of  $K_1$ ,  $K_2$ ,  $V_1$ , and  $V_2$ :

$$\alpha = 1/(V_1 + V_2)$$

$$\beta = K_1 K_2/(K_1 V_2 + K_2 V_1)$$

$$\gamma = V_1 V_2 (K_1 - K_2)^2 / ((V_1 + V_2)^2 (K_1 V_2 + K_2 V_1))$$

$$\delta = (K_1 V_2 + K_2 V_1)/(V_1 + V_2).$$

The differential equation (2) can easily be solved, resulting in an expression describing  $t$  as a function

of  $S$  (the more straightforward way of expressing  $S$  in terms of  $t$  being impossible in this case):

$$t = \alpha(S_0 - S) + \beta \ln(S_0/S) + \gamma \ln((\delta + S_0)/(\delta + S)) \quad (3)$$

where  $S_0$ , as usual, is the substrate concentration at  $t = 0$ . The average rate of change over the time interval  $(0, t_1)$  is

$$\bar{r} = (S_0 - S_1)/t_1. \quad (4)$$

By means of Eqn. (3)  $t_1$  can be expressed in  $S_1$ , resulting in

$$\frac{1}{\bar{r}} = t_1/(S_0 - S_1) = \alpha + (\beta/(S_0 - S_1)) \ln(S_0/S_1) + (\gamma/(S_0 - S_1)) \ln((\delta + S_0)/(\delta + S_1)). \quad (5)$$

Some time between 0 and  $t_1$  there must be an instant  $x$  and a corresponding substrate concentration  $S_x$  at which the rate of change  $v_x$  equals the average rate of change  $\bar{r}$ .  $S_x$  can be solved from the equation  $v_x = \bar{r}$ , or, equivalently,

$$\frac{1}{v_x} = \frac{1}{\bar{r}}. \quad (6)$$

Equation (6) can be solved by inserting Eqn. (2) and Eqn. (5). This results in a quadratic equation in  $S_x$ :

$$\frac{1}{(S_0 - S_1)} \left( \beta \ln \frac{S_0}{S_1} + \gamma \ln \frac{\delta + S_0}{\delta + S_1} \right) S_x^2 + \left\{ \frac{\delta}{S_0 - S_1} \left( \beta \ln \frac{S_0}{S_1} + \gamma \ln \frac{\delta + S_0}{\delta + S_1} \right) - \beta - \gamma \right\} S_x - \beta \delta = 0. \quad (7)$$

Analysis of the coefficients shows that there is always precisely one positive – in order words: physically meaningful – solution for  $S_x$ . Equation

(7) can be rearranged in a quadratic equation in  $S_x/S_0$ :

$$\frac{A(\varphi + 1)}{(1 - \varepsilon)(\varphi + \kappa)} \left( \frac{S_x}{S_0} \right)^2 + \left\{ \frac{A}{\zeta(1 - \varepsilon)} - \frac{(\varphi \kappa + 1)}{(\varphi + 1)} \right\} \left( \frac{S_x}{S_0} \right) - \frac{\kappa}{\zeta} = 0 \quad (8)$$

where  $\varepsilon = S_1/S_0$ ;  $\zeta = S_0/K_1$ ;  $\kappa = K_2/K_1$ ;  $\varphi = V_2/V_1$  and

$$A = -\kappa \ln \varepsilon + \frac{\varphi(1 - \kappa)^2}{(\varphi + 1)^2} \ln \frac{\varphi + \kappa + \zeta(\varphi + 1)}{\varphi + \kappa + \varepsilon \zeta(\varphi + 1)}.$$

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